

## Transient analysis of the release and reduction of NO<sub>x</sub> using a Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalyst

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### Abstract

The release and reduction of NO<sub>x</sub> in a NO<sub>x</sub> storage-reduction (NSR) catalyst were studied with a transient reaction analysis in the millisecond range, which was made possible by the combination of pulsed injection of gases and time resolved time-of-flight mass spectrometry. After an O<sub>2</sub> pulse and a subsequent NO pulse were injected into a pellet of the Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalyst, the time profiles of several gas products, NO, N<sub>2</sub>, NH<sub>3</sub> and H<sub>2</sub>O, were obtained as a result of the release and reduction of NO<sub>x</sub> caused by H<sub>2</sub> injection. Comparing the time profiles in another analysis, which were obtained using a model catalyst consisting of a flat 5 nmPt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite plate, the release and reduction of NO<sub>x</sub> on Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalyst that stored NO<sub>x</sub> took the following two steps; in the first step NO molecules were released from Ba and in the second step the released NO was reduced into N<sub>2</sub> by H<sub>2</sub> pulse injection. When this H<sub>2</sub> pulse was injected in a large amount, NO was reduced to NH<sub>3</sub> instead of N<sub>2</sub>.

A only small amount of H<sub>2</sub>O was detected because of the strong affinity for alumina support. We can analyze the NO<sub>x</sub> regeneration process to separate two steps of the NO<sub>x</sub> release and reduction by a detailed analysis of the time profiles using a two-step reaction model. From the result of the analysis, it is found that the rate constant for NO<sub>x</sub> release increased as temperature increase.

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**Keywords:** Time-of-flight mass spectrometry; NSR catalyst; Cordierite plate

### 1. Introduction

Lean-burn and diesel engines have great potentials in overcoming the problems of environmental pollution and fuel economy. However, conventional three-way catalysts are ineffective in removing NO<sub>x</sub> from the exhaust gas of these engines, which contains a large amount of oxygen. One effective method that solves this problem is the use of a NO<sub>x</sub> storage-reduction (NSR) catalyst [1–5].

NSR catalysts remove NO<sub>x</sub> by alternating the composition of the exhaust gas between lean and rich. During the lean period of operation, the catalyst stores NO<sub>x</sub> as species of nitrites and nitrates. A short pulse of rich gas is injected so that the stored NO<sub>x</sub> is released and reduced to N<sub>2</sub>. It is generally accepted that this NSR process can be separated into five elemental reactions [6,7]:

- (1) NO oxidation to NO<sub>2</sub> [8,9].
- (2) NO<sub>x</sub> storage on the catalyst surface [10,11].
- (3) Evolution of reductant.
- (4) NO<sub>x</sub> release from the storage site.
- (5) NO<sub>x</sub> reduction to N<sub>2</sub>.

Despite the general acceptance of this process, the detailed mechanisms are not fully understood, especially the release and reduction of NO<sub>x</sub>. From a practical point of view, it has been reported that at relatively low temperature the NO<sub>x</sub> storage capacity is sufficient, but that the rate of NO<sub>x</sub> release and reduction, sometimes called the NO<sub>x</sub> regeneration, is slow and insufficient [12]. Analysis of the NO<sub>x</sub> regeneration is more difficult than that of NO oxidation and NO<sub>x</sub> storage, because the regeneration accompanied by pulse injection of rich gas is completed in an extremely short period. Another reason for this difficulty is that the main reaction product is N<sub>2</sub>, which is a significant constituent in real exhaust gases and is usually used for the diluent gas in the laboratory.

Although some studies of transient reaction have been done using He as a diluent gas [10,13–15], it seems that with this

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method the time resolution of the measurement was too low even to obtain the time profile of the main product,  $N_2$ . The aim of the present study is to develop a method to obtain the time profile of  $N_2$  with millisecond resolution. Moreover, we would like to improve our understanding of the  $NO_x$  regeneration process.

Motohiro et al. developed a dynamic vacuum system for transient reaction analysis of a flat type catalyst on a millisecond timescale (which is essentially a time-resolved time-of-flight mass spectrometry with molecular-pulse-probe for reaction analysis at the surface of catalysts named TM+ since the output raw data is essentially the amount of reaction product cations (+) mapped on the time (T) and mass (M) space) [16–18]. The TM+ system has also blanchet out to analyze the transient reaction of a pellet type catalyst [19,20] by reference to the TAP (temporal analysis of products) reactor [21]. We applied both reactor systems in our NSR analysis.

## 2. Experimental

### 2.1. Preparation of a Pt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite plate for analyzing the decomposition of Ba(NO<sub>3</sub>)<sub>2</sub>

Pt and Ba were chosen, respectively, as the precious metal and the  $NO_x$  storage component for our study because they are well-accepted materials for NSR catalysts.

We prepared two kinds of samples for our study, a flat sample and a pellet sample. The latter is described in the next section. The flat sample, 5 nmPt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite, was fabricated starting with a square cordierite plate, 50 mm on a side and 5 mm thickness. A saturated solution of Ba(NO<sub>3</sub>)<sub>2</sub> (Wako Pure Chemical Industries) of 5 cm<sup>3</sup> was dropped onto the plate, which was then dried in vacuum at room temperature overnight. The resultant sample was then placed in an ultra high vacuum chamber and was sputter-coated with platinum at the amount equivalent to 5 nm in thickness. The resultant sample named 5 nmPt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite plate was deemed to be a model NSR catalyst, saturated with sites for  $NO_x$  storage.

### 2.2. Preparation of a pellet type Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalysts for NSR analyses

Pellets of Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalyst were prepared using a two-step wet impregnation method. Firstly, powdery  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (Nikki Universal, 150 m<sup>2</sup>/g) was wet impregnated with Pt(NH<sub>3</sub>)<sub>2</sub>(NO<sub>2</sub>)<sub>2</sub> (Tanaka Precious Metals). This material was filtered, washed, dried at 393 K for 12 h, and calcined at 573 K for 3 h in the air. We call this a Pt/Al<sub>2</sub>O<sub>3</sub> sample. Secondly, a portion of this sample was stirred into an aqueous solution containing Ba(CH<sub>3</sub>COO)<sub>2</sub> (Wako Pure Chemical Industries) and the excess water was removed by heating while continually stirring. The resultant powder was dried at 393 K for 12 h and calcined at 773 K for 3 h in the air. The amount of Pt and Ba per 120 g  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> was 2 g and 0.2 mol, respectively. The powder sample was pressed and sieved to make pellets of 0.7–1.0 mm diameter.

### 2.3. Transient reaction analysis of a flat type catalyst

A flat plate sample of 5 nmPt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite was placed in the TM+ apparatus shown in Fig. 1. The apparatus was equipped with four pulsed valves, two cryopumps for vacuum chambers placed sample, and two turbo pumps for differentially pumped down chambers and time-of-flight mass spectrometer (TOF-MS). The sample was fixed in a holder with a flat heater and the surface temperature was maintained at 350 °C. Pulses of pure H<sub>2</sub> gas with a volume of 0.2 cm<sup>3</sup> and pulse width of 1 ms were supplied to release and reduce the Ba(NO<sub>3</sub>)<sub>2</sub> in the sample. The reason for choosing H<sub>2</sub> was because this is the most effective gas for regeneration of stored  $NO_x$  at low temperature [22] and because its simple mass peaks of H<sub>2</sub> and prospective products makes the analysis of the mass spectra easy. The chambers were kept under high vacuum: the first chamber, where the samples were placed, was at about 10<sup>−6</sup> Pa; the differential chamber at 10<sup>−7</sup> Pa, and the chamber for TOF-MS at 10<sup>−8</sup> Pa. The intensity of each mass peak was calibrated using mass spectral data [23].

The measurement procedure was as follows. After injecting pulse of H<sub>2</sub>, a part of the reaction products emitted from the catalyst was sampled through a skimmer located in the direction normal to the plane surface of the catalyst. The reaction products were ionized and detected by the TOF-MS on a millisecond scale. This procedure of H<sub>2</sub> gas pulsing and detection of the gas products was repeated 100 times with a period of 5 s in order to improve the signal to noise ratio by averaging the accumulated data. The amount of reaction products and  $NO_x$  in the sample decreased gradually as the progress of Ba(NO<sub>3</sub>)<sub>2</sub> decomposition by H<sub>2</sub> gas pulsing because  $NO_x$  was not supplied to the sample during the measurement. The averaging data were the result of the averaging of the products for 100 times of the measurement, though the amount of the products of each measurement was decreased as the progress of Ba(NO<sub>3</sub>)<sub>2</sub> decomposition. The elemental ratio of the sample surface was measured by X-ray photoelectron spectroscopy (XPS) before and after the H<sub>2</sub> pulsing experiment.

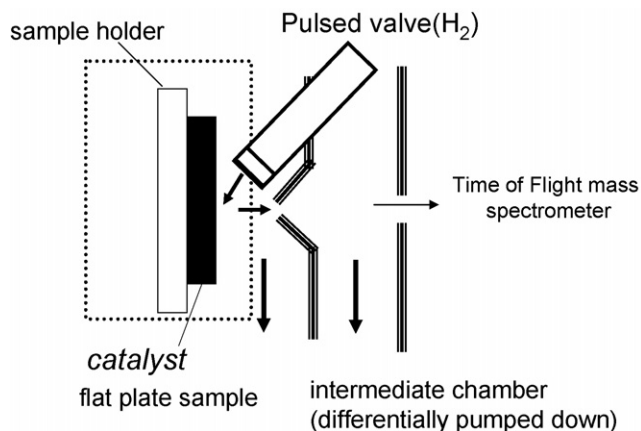


Fig. 1. TM+ apparatus for a flat plate sample. Pulses of reactant gases are supplied through valves. The catalyst sample is set in ultra high vacuum conditions. The gases are analyzed with time-of-flight mass spectrometry through a differentially pumped-down intermediate chamber.

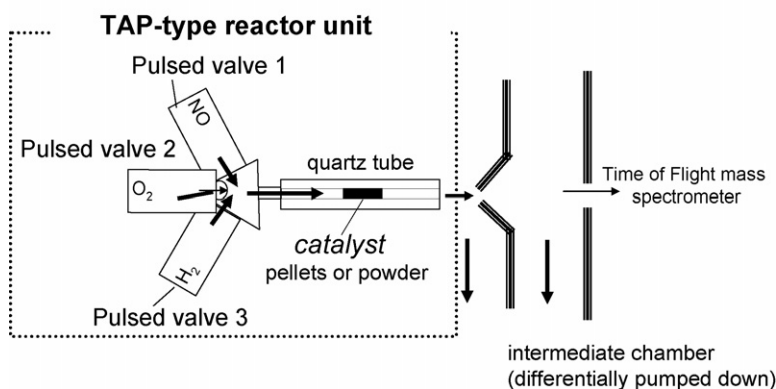


Fig. 2. TAP-type reactor apparatus for NSR analysis. Pulses of the reactant gases, NO, O<sub>2</sub> and H<sub>2</sub>, are supplied through three separate valves. Catalyst in the form of pellets or powder is placed into a quartz tube. The gases are analyzed in the same way as shown in Fig. 1.

#### 2.4. Transient reaction analysis of a pellet type catalyst

A 0.2 g pellet of Pt/Ba/Al<sub>2</sub>O<sub>3</sub> catalyst was inserted into a quartz tube with a 4.5 mm internal diameter and a length of 38 mm, as shown in Fig. 2. Silica wool was stuffed into both ends of the quartz tube. A simplified schematic diagram of the TAP-type reactor apparatus is shown in Fig. 2 [19,20], which is installed in the TM+ system mentioned in Section 2.3. The quartz tube containing the catalyst was installed in this vacuum system, which was evacuated to 10<sup>−7</sup> Pa. The tube was then heated with an external heater up to a preset temperature. For this analysis, we used three valves for the gas pulses, one each for pure O<sub>2</sub>, NO and H<sub>2</sub> gases. The amount of gas in the pulse could be controlled either by the pulse width or by the backpressure of the valve. In this case, the amount of gas was controlled by the backpressure of the valve. The measured pulse width was broader than 1.0 ms preset by a pulsed valve controller because of a gas diffusion effect; nevertheless all the pulse widths were set to 1.0 ms by a pulsed valve controller. The amount of O<sub>2</sub> and NO was fixed at about 0.8 and 1.0 cm<sup>3</sup> per pulse, respectively. The amount of Ba for NO<sub>x</sub> storage was calculated to be 3 × 10<sup>−7</sup> mol per 0.2 g catalyst, whereas the amount of NO was 3 × 10<sup>−4</sup> mol per pulse. Thus, the amount of NO was altogether sufficient for the amount of Ba. The amount of H<sub>2</sub> was varied from 0.1 to 0.4 cm<sup>3</sup> per pulse by changing the backpressure of the valve.

The measurement procedure used for this analysis was similar to that used for TM+ type analysis of the flat type catalyst in Section 2.3, and was as follows. After maintaining the catalyst at a preset temperature, an O<sub>2</sub> pulse was injected to the catalyst followed by a NO pulse injection with an interval of 100 ms. This procedure models the NO<sub>x</sub> storage step, which involves oxidation of NO into NO<sub>2</sub> and storage of NO<sub>x</sub>. H<sub>2</sub> was injected to the catalyst 5 s after the injections of O<sub>2</sub> and NO pulses in order to bring about NO<sub>x</sub> regeneration. The NO<sub>x</sub> storage step was repeated again 200 ms after the H<sub>2</sub> injection. The NO<sub>x</sub> storage and regeneration was repeated 30 times in order to improve the signal to noise ratio as was done for the analysis of the flat type catalyst. The reactant and product gases were detected for 200 ms after the O<sub>2</sub> pulse injection and for 200 ms after the H<sub>2</sub> pulse injection. In order to accumulate data after the reaction stabilized, the same measurement procedure was repeated 30 times as a pretreatment.

### 3. Results

#### 3.1. Ba(NO<sub>3</sub>)<sub>2</sub> decomposition analysis

H<sub>2</sub>O, NH<sub>3</sub>, N<sub>2</sub> and NO were detected with H<sub>2</sub> injection to the flat sample of the 5 nmPt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite in the TM+ type measurement as shown in Fig. 3, however N<sub>2</sub>O and NO<sub>2</sub> were not detected. When the Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite without Pt was also

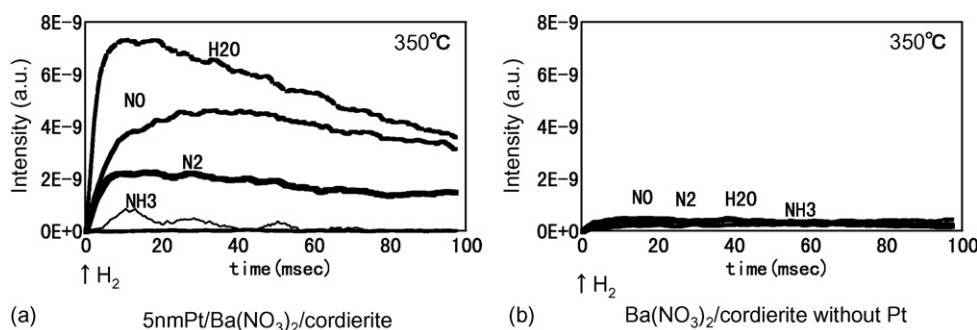


Fig. 3. Time profiles of the gas products generated as a result of Ba(NO<sub>3</sub>)<sub>2</sub> decomposition from supplying pulses of H<sub>2</sub> gas to: (a) a flat type sample of 5 nmPt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite (2MgO·2Al<sub>2</sub>O<sub>3</sub>·5SiO<sub>2</sub>) and (b) a flat type sample of Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite without Pt at 350 °C in TM+ type measurement.

Table 1

Surface elemental composition measured with XPS before and after the  $\text{Ba}(\text{NO}_3)_2$  decomposition experiment of 5 nmPt/ $\text{Ba}(\text{NO}_3)_2$ /cordierite

	Surface elemental composition (%)					N/Ba ratio
	Pt	Ba	N	C	O	
Before	36	3.1	4.0	36	21	1.29
After	15	9.1	4.5	32	40	0.49

analyzed to investigate the role of Pt, none of these products were detected. This indicated clearly that Pt was necessary to release  $\text{NO}_x$  from  $\text{Ba}(\text{NO}_3)_2$  by  $\text{H}_2$ . This essential role of Pt for regeneration of  $\text{NO}_x$  was also elucidated recently by an analysis with in situ Fourier Transform Infrared spectroscopy [24]. It was found that both  $\text{NO}_x$  storage and regeneration needs Pt because the role of Pt of  $\text{NO}$  oxidation to  $\text{NO}_2$  in  $\text{NO}_x$  storage process has been well known [25].

The surface elemental composition of the 5 nmPt/ $\text{Ba}(\text{NO}_3)_2$ /cordierite was measured using XPS before and after the above experiment as shown in Table 1. The reduction in the N/Ba ratio after the experiment confirmed the decomposition of  $\text{Ba}(\text{NO}_3)_2$ . When comparing the surface elemental composition before and after the measurement, it was found that the percentage of Pt decreased while the percentage of Ba increased. It is considered that the sintering of the Pt particles and encapsulation of the Pt particles cause the compositional change. The Pt in the  $\text{Ba}(\text{NO}_3)_2$ /cordierite was unstable and easily sintered into large particles. The phenomenon of the encapsulation of Pt particles by Ba has been observed after the reduction of a barium-based NSR catalyst [26].

### 3.2. Comparison of Pt/Ba/ $\text{Al}_2\text{O}_3$ with Pt/ $\text{Al}_2\text{O}_3$ in the TAP-type analyses

The results of TAP-type analyses of NSR using the pellet samples of Pt/Ba/ $\text{Al}_2\text{O}_3$  and Pt/ $\text{Al}_2\text{O}_3$  at 310 °C are shown in Fig. 4. When comparing the profile of  $\text{NO}$  and  $\text{O}_2$  of Pt/Ba/ $\text{Al}_2\text{O}_3$  to the one of Pt/ $\text{Al}_2\text{O}_3$  (Fig. 4(a and c)), both the signal intensities of  $\text{NO}$  and  $\text{O}_2$  of Pt/Ba/ $\text{Al}_2\text{O}_3$  were less than the one of Pt/ $\text{Al}_2\text{O}_3$ . The product gases with  $\text{H}_2$  injection as the result of NSR reaction were found in the case of Pt/Ba/ $\text{Al}_2\text{O}_3$ . These results indicated that the  $\text{NO}_x$  was stored in Pt/Ba/ $\text{Al}_2\text{O}_3$  and the NSR reaction took place only in the case of Pt/Ba/ $\text{Al}_2\text{O}_3$ . In our experiment of Pt/ $\text{Al}_2\text{O}_3$ , the adsorption of  $\text{NO}_x$  on the Pt and  $\text{Al}_2\text{O}_3$  [27,28] was not found.

Even though a large amount of  $\text{NO}$  and  $\text{H}_2\text{O}$  were observed in the TM+ type experiment using the 5 nmPt/ $\text{Ba}(\text{NO}_3)_2$ /cordierite sample (Fig. 3),  $\text{NO}$  was not observed here but a small amount of  $\text{H}_2\text{O}$  was. We suppose that almost all the  $\text{NO}$  was reduced to  $\text{N}_2$  or  $\text{NH}_3$  immediately and that the  $\text{H}_2\text{O}$  desorbed very slowly because of the strong affinity for alumina support. Therefore, the rate-limiting step during the rich phase is the decomposition of barium nitrate [29].

### 3.3. Influence of the amount of $\text{H}_2$

The influence of the amount of  $\text{H}_2$  was investigated at 310 °C (Fig. 5). The amounts and ratios of the product and reactant gases changed in response to the increase in the amount of  $\text{H}_2$  from 0 to 0.4  $\text{cm}^3$ .  $\text{NO}$  and  $\text{O}_2$  decreased and  $\text{NH}_3$  increased with the amount of  $\text{H}_2$  injection on the case between 0 and 0.3  $\text{cm}^3$   $\text{H}_2$  injection. In the case of 0.4  $\text{cm}^3$

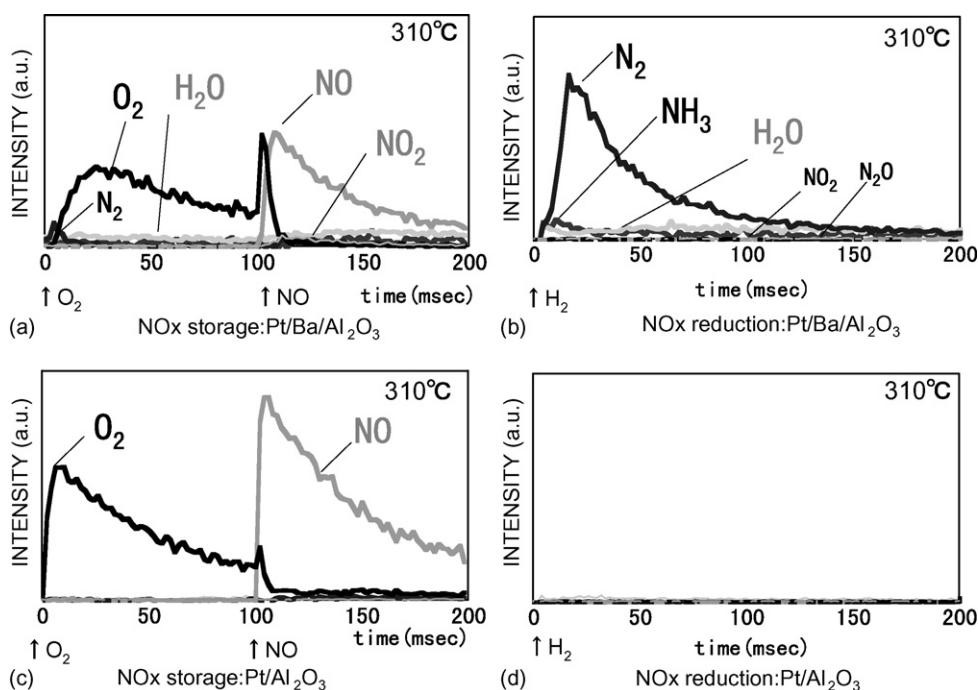


Fig. 4. TAP-type NSR analysis of Pt/Ba/ $\text{Al}_2\text{O}_3$  and Pt/ $\text{Al}_2\text{O}_3$  at 310 °C: (a)  $\text{NO}_x$  is stored in the Pt/Ba/ $\text{Al}_2\text{O}_3$ ; (b) the stored  $\text{NO}_x$  is reduced by the 0.2  $\text{cm}^3$  pulses of  $\text{H}_2$  gas, which is supplied 5 s after the  $\text{NO}_x$  storage procedure; (c and d) Pt/ $\text{Al}_2\text{O}_3$  does not show the activity of NSR.



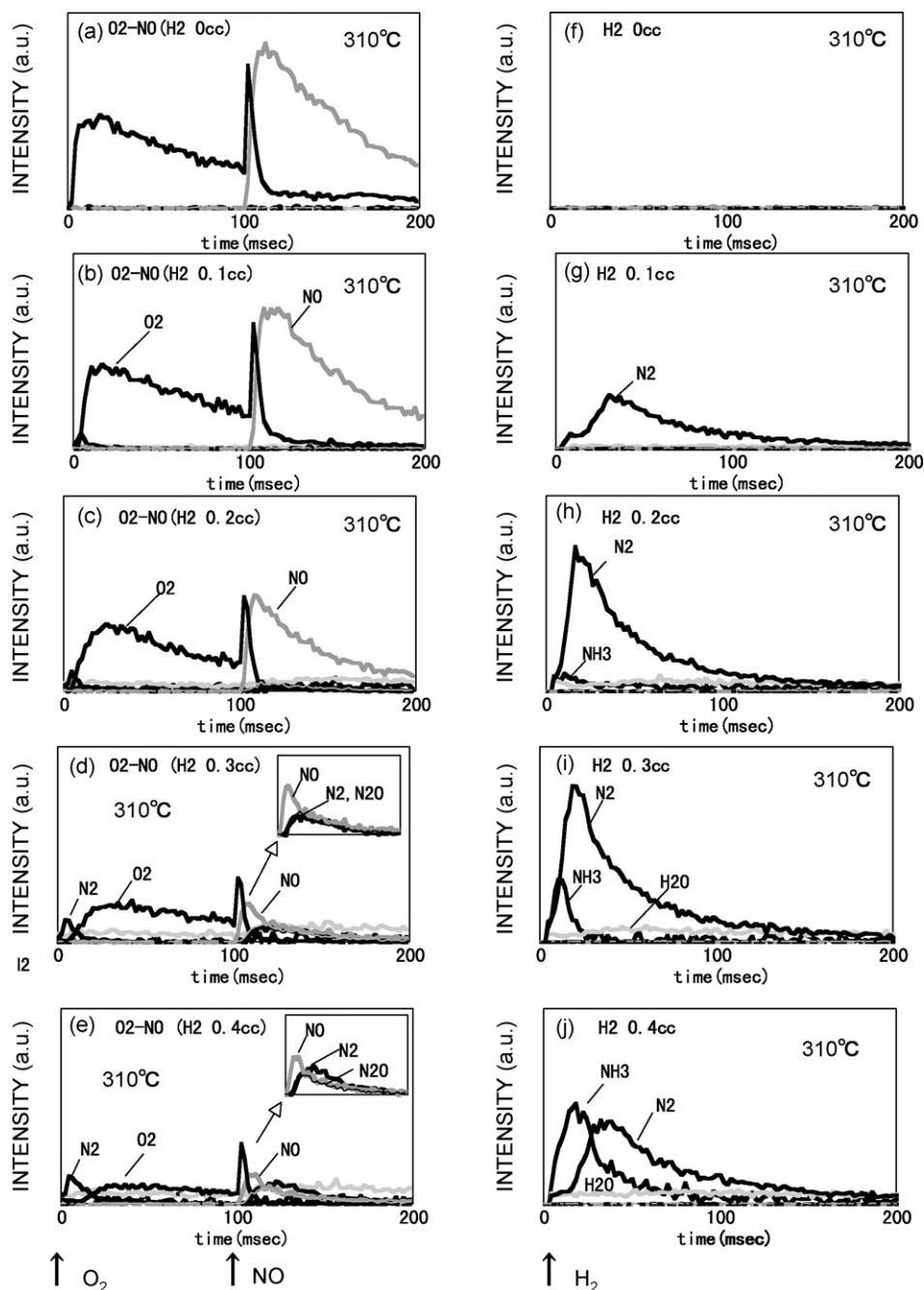


Fig. 5. Effect of the amount of  $H_2$  on the NSR of Pt/Ba/ $Al_2O_3$  at 310 °C. NO decreases and  $NH_3$  increases with increasing amount of  $H_2$ .

$H_2$  injection (Fig. 5(j)), the amount of  $NH_3$  increased and the amount of  $N_2$  decreased in comparison with the result in Fig. 5(i).

We would like to just refer  $N_2$  and  $N_2O$  after the injection of NO. In the case of 0.3 and 0.4  $cm^3$   $H_2$  injection,  $N_2$  and  $N_2O$  were found after the injection of a NO pulse as shown in the magnified views in Fig. 5(d and e). When NO was injected, some of the injected NO was reduced to  $N_2$  and  $N_2O$  at the Pt surface, which was still reduced or absorbed hydrogen despite the previous injection of  $O_2$ . This reaction was same as  $NO_x$  selective reduction and  $NO_x$  direct reduction.

### 3.4. Influence of temperature

We also investigated the influence of the amount of  $H_2$  on both the products and reactants associated with  $NO_x$  storage and regeneration at temperatures of 440, 360, 310, 270 and 230 °C. In Fig. 6, the results are displayed in such a manner that the temperature varies in the vertical direction and the amount of  $H_2$  varies in the horizontal direction. The  $N_2$  intensity and the half of the  $NH_3$  intensity were plotted against time. The leading edge of the time profile is generally steeper with increasing  $H_2$  gas volume and increasing temperature. The ratio of  $NH_3$  to  $N_2$  also increases in the same way. We will discuss the rate of  $NO_x$

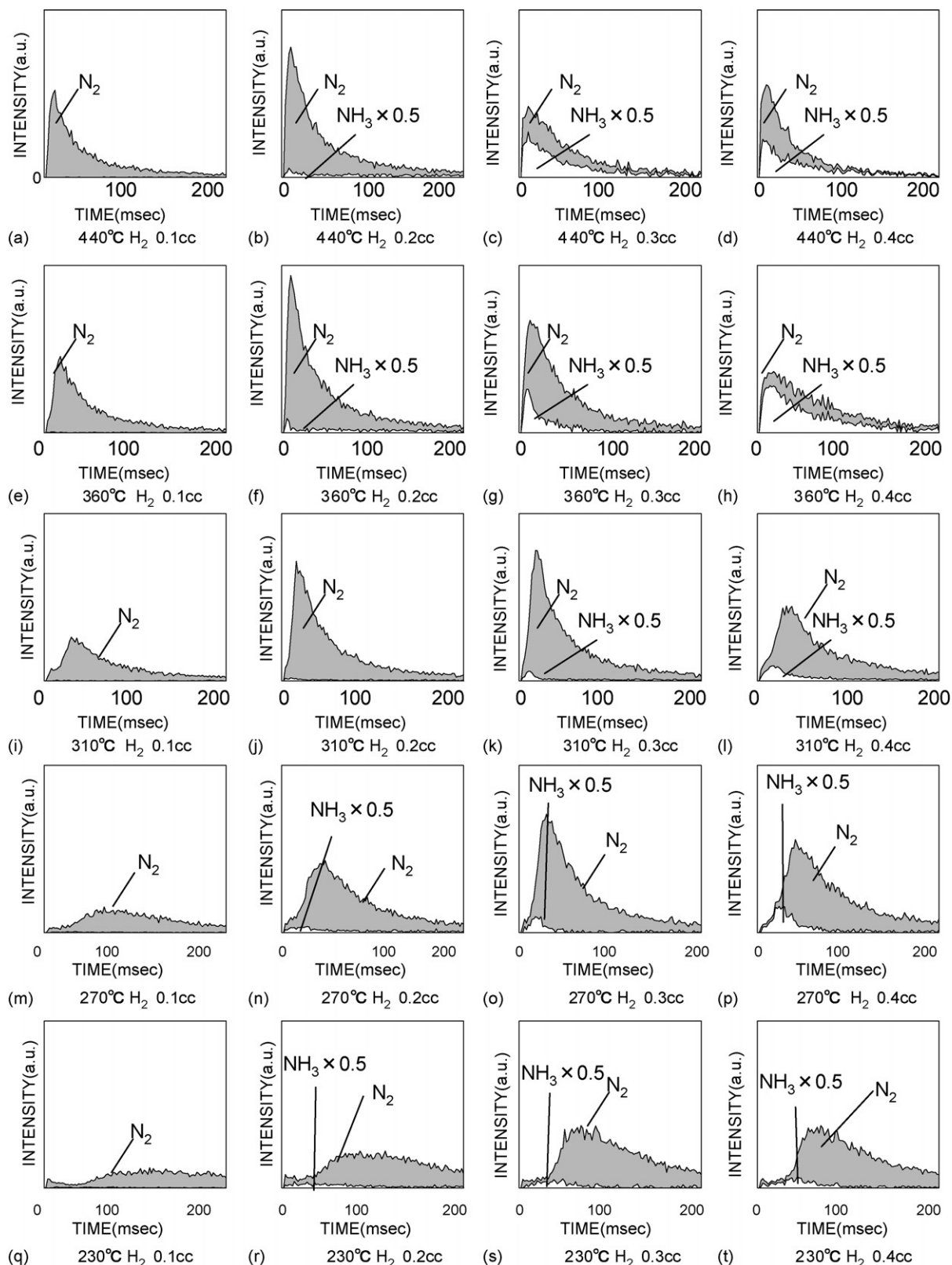


Fig. 6. Effect of temperature and amount of  $H_2$  gas pulse on the time profiles of  $N_2$  and  $NH_3$  after supplying pulses of  $H_2$  gas to Pt/Ba/ $Al_2O_3$ .

release and reduction, and the formation of  $NH_3$  in the next section.

The amount of reduced  $NO_x$  was calculated at each temperature by subtracting NO profile of each amount of  $H_2$

injection from the NO profile of 0  $cm^3$  of  $H_2$  injection (Fig. 7). In the case of 0.3 and 0.4  $cm^3$   $H_2$  injection, the results agree with the previously known fact that the amount of  $NO_x$  storage is largest around 350 °C [11,30].

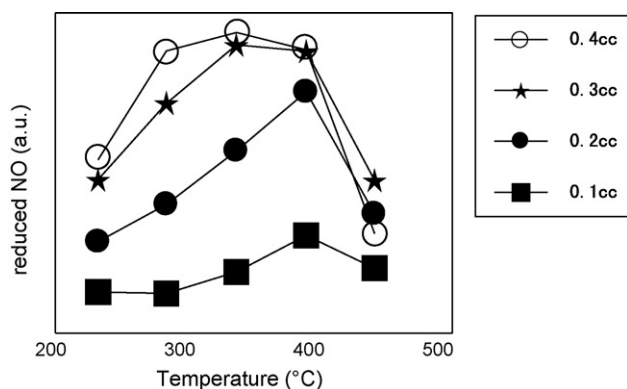


Fig. 7. Amount of reduced NO in the NSR analysis of Pt/Ba/Al<sub>2</sub>O<sub>3</sub>. The amount of reduced NO was calculated from the NO profile obtained from the analysis. The profiles are very similar to those of previously reported studies of NSR catalysts by conventional method.

#### 4. Discussion

A NSR reaction with H<sub>2</sub> gas was investigated on a millisecond time scale using a flat 5 nmPt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite catalyst and a pellet of Pt/Ba/Al<sub>2</sub>O<sub>3</sub>. Instead of the direct comparison of the NO<sub>x</sub> regeneration rate, we compared the

profiles of  $[N_2 + NH_3/2]$ : the sum intensity of N<sub>2</sub> and half of NH<sub>3</sub>. The profiles at each temperature were chosen so as to give almost the same amount of reduced NO<sub>x</sub>, namely, 0.3, 0.2, 0.2, 0.2 and 0.3 cm<sup>3</sup> at 440, 360, 310, 270 and 230 °C, respectively (Fig. 8(a)). The  $[N_2 + NH_3/2]$  increased as the temperature increases from 230 to 360 °C as described in the previous section and shown in Fig. 7. It was found that the NO<sub>x</sub> regeneration rate became faster with increasing temperature, as shown by the leading edge of the normalized peak values becoming more rapid as the temperature increases (Fig. 8(b)).

To make the difference of the NO<sub>x</sub> regeneration rate clearer, we tried to fit theoretical curves obtained from a simple reaction model to the  $[N_2 + NH_3/2]$  profiles with a least square method. We assumed a two-step reaction model, whose formula was described as follows [31];

$$\frac{dC}{dt} = \frac{K_1 K_2}{(K_1 - K_2)} C_0 (\exp(-K_2 t) - \exp(-K_1 t)).$$

Here,  $t$  stands for time and  $dC/dt$  stands for the intensity:  $[N_2 + NH_3/2]$ . The  $K_1$  stands for the rate constant of the first step reaction and the  $K_2$  stands for the one of the second step.  $C_0$  is considered as the concentration of the stored NO<sub>x</sub>. If we

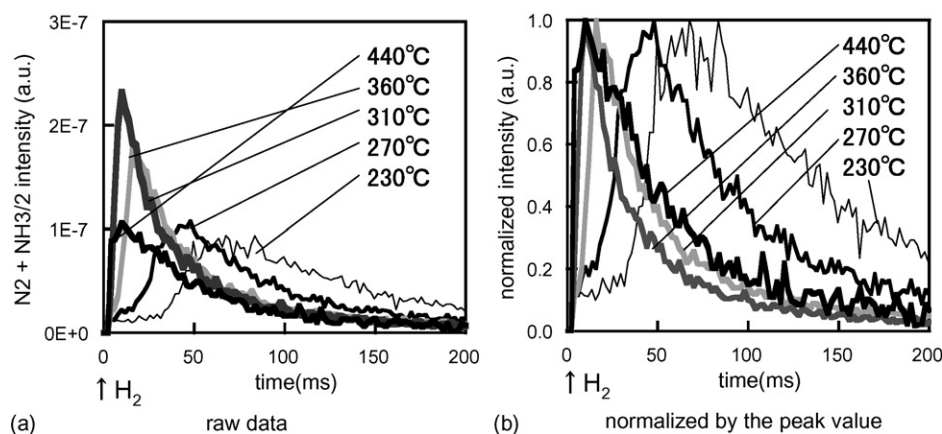


Fig. 8. Comparison of the N<sub>2</sub> + NH<sub>3</sub>/2 profile (a) raw data and (b) normalized by the peak value.

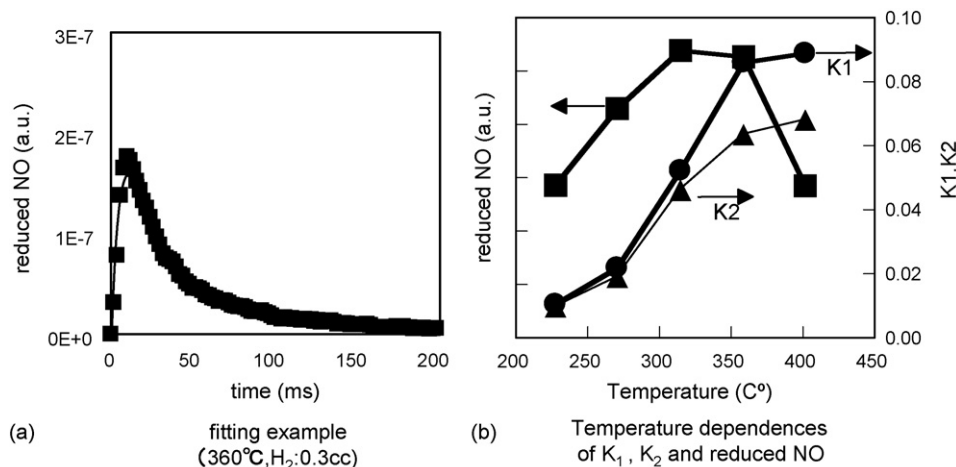


Fig. 9. Temperature dependences of the speed of NO<sub>x</sub> regeneration and the amount of NO<sub>x</sub> reduced using the data of 0.3 cm<sup>3</sup> of H<sub>2</sub> injection: (a) a fitting example of N<sub>2</sub> + NH<sub>3</sub>/2 profile at 360 °C and (b) temperature dependences of  $K_1$ ,  $K_2$  and reduced NO: the same data in Fig. 7.

assume the first step as NO<sub>x</sub> release and the second step as NO<sub>x</sub> reduction, we are able to have the each rate constant.

An example of the fitting was shown in Fig. 9(a). The fitting seems to be successful. This fitting was performed to other time profiles of 0.3 cm<sup>3</sup> of H<sub>2</sub> injection. As shown in Fig. 9(b), the temperature dependences of  $K_1$ ,  $K_2$  and the amount of reduced NO for 0.3 cm<sup>3</sup> H<sub>2</sub> injection. The rate constant of  $K_1$  and  $K_2$  increased with increase in temperature from 230 to 440 °C, while the temperature dependence of the amount of reduced NO<sub>x</sub> shows a maximum value around 300 °C. From this analysis, we suppose that the amount of reduced NO<sub>x</sub> was decreased above 360 °C because of the decrease of the NO<sub>x</sub> storage reactivity in Pt/Ba/Al<sub>2</sub>O<sub>3</sub>. If we assume the first step as NO<sub>x</sub> release and the second step as NO<sub>x</sub> reduction as mentioned above, it is considered that the rate constant of NO<sub>x</sub> release and NO<sub>x</sub> reduction between 230 and 310 °C are almost the same. When the temperature increase over 360 °C, the rate constant for NO<sub>x</sub> release was found to be larger than the one for NO<sub>x</sub> reduction. When the temperature was increased to 440 °C, a large amount of NH<sub>3</sub> was yielded. This NH<sub>3</sub> formation may be connected with the small rate of NO<sub>x</sub> reduction over 360 °C.

At last, we would like to discuss NO storage reaction in NSR reaction and NH<sub>3</sub> formation in NO<sub>x</sub> regeneration. It is clear that the profiles of O<sub>2</sub> and NO are different in the NO<sub>x</sub> storage process shown in Fig. 5. The leading edge of the O<sub>2</sub> profile became gentler as the amount of H<sub>2</sub> increased, but the leading edge of the NO profile remained stable. This difference may indicate the difference between the reaction mechanisms of O<sub>2</sub> and NO with Pt/Ba/Al<sub>2</sub>O<sub>3</sub>, i.e., O<sub>2</sub> reacted with Pt/Ba/Al<sub>2</sub>O<sub>3</sub> very fast and NO did not. When O<sub>2</sub> is injected to the Pt/Ba/Al<sub>2</sub>O<sub>3</sub>, the surface reduced by H<sub>2</sub> can adsorb O<sub>2</sub> immediately. However, NO needs to react with dissociated oxygen for NO<sub>x</sub> storage [32–34] and therefore the rate of NO reaction was not faster than the one of O<sub>2</sub> reaction.

A detailed report on NO<sub>x</sub> regeneration in a NSR catalyst was recently published [35]. Although the report focused mainly on the effect of different reducing agents and precious metals, NH<sub>3</sub> formation in NO<sub>x</sub> regeneration is also discussed. The result of the discussion showed that the amount of NH<sub>3</sub> increased as the temperature increased, which is the same as the result found in this work (Fig. 6). Another analysis showed that the generation of N<sub>2</sub> and the subsequent generation of NH<sub>3</sub> [36] accompany the introduction of H<sub>2</sub>. The order in which these gases were generated is opposite to our result. The difference may be presumably due to the difference in the methods of H<sub>2</sub> introduction, i.e., pulsed injection in our case and step injection in the reference [36] in which the time profile of induced H<sub>2</sub> increases rapidly and then becomes stable. NH<sub>3</sub> formation tends to occur when the ratio of H<sub>2</sub> to NO increases [37]. In our study, the H<sub>2</sub>/NO ratio is high just after H<sub>2</sub> pulse injection because the H<sub>2</sub> concentration is considered to be highest at that time and decreases rapidly from then on. On the other hand, in the study using a step profile for H<sub>2</sub>, the H<sub>2</sub>/NO ratio is low just after injection because a large amount of NO exists in the catalyst and the H<sub>2</sub>/NO ratio is considered to increase gradually from then on. We regard this as the reason why the order of N<sub>2</sub> and NH<sub>3</sub> generation was different between the two works.

The formation of NH<sub>3</sub> and intermediate gases caused by CO and hydrocarbons [38] has often been discussed. This can be neglected in our case, because these reducing agents were not used in this study. However, the NH<sub>3</sub> may play an important role in NO<sub>x</sub> release and reduction. Further analysis is necessary such as using NH<sub>3</sub> directly as a reducing agent for stored NO<sub>x</sub>.

## 5. Conclusions

NO<sub>x</sub> regeneration in an NSR catalyst with H<sub>2</sub> gas was investigated on a millisecond time scale. As for the gases produced as a result of NO<sub>x</sub> regeneration, NO, N<sub>2</sub>, NH<sub>3</sub> and H<sub>2</sub>O, were detected from a flat 5 nmPt/Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite catalyst, though no products were detected from Ba(NO<sub>3</sub>)<sub>2</sub>/cordierite. It was found that Pt plays an important role in the NSR reaction and that NO was produced from decomposition of Ba(NO<sub>3</sub>)<sub>2</sub> in the catalyst.

A NSR reaction using a pellet of Pt/Ba/Al<sub>2</sub>O<sub>3</sub> as the catalyst was also investigated. The results were different from the analysis using the flat catalyst in which only a small amount of H<sub>2</sub>O was detected because of the strong affinity for alumina support. NO was not observed since it was reduced into N<sub>2</sub>. For a large amount of H<sub>2</sub> injection, a large amount of NH<sub>3</sub> was detected. Analysis both of the N<sub>2</sub> profile and their leading edges showed that the rate of NO<sub>x</sub> regeneration increased with temperature and the amount H<sub>2</sub>. We can analyze the NO<sub>x</sub> regeneration process to separate two steps of the NO<sub>x</sub> release and reduction by a detailed analysis of the time profiles using a two-step reaction model. From the result of the analysis, it is found that the rate constant for NO<sub>x</sub> release increased as temperature increase.

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